## Appendix 1

Traffic Forecasting Memorandum

STEVE SISOLAK
state of nevada
DEPARTMENT OF TRANSPORTATION
1263 S. Stewart Street
Carson City, Nevada 89712

Governor

KRISTINA L. SWALLOW, P.E., Director
In Reply Refer to:

February 13, 2020

Mr. John Karachepone, P.E.
Jacobs Engineering Group Inc
250 Pilot Road, Suite 160
Las Vegas, Nevada 89119
Dear Mr. Karachepone:
The Nevada Department of Transportation's Traffic Information Section has reviewed the forecasting methodology and traffic volumes used in the I-515/I-215 Interchange Feasibility Study Traffic Forecasting Memorandum produced by John Karachepone of Jacobs dated February 11, 2020. The current and future traffic volumes seem reasonable for use in the traffic operation analysis. Should you require clarification or additional information please contact myself or Chris Wright at (775) 888-7443.

Sincerely,


CC: Hoang Hong, Traffic Operations
Sam Ahiamadi, Traffic Operations
Dave Bowers, NDOT Project Manager

## Technical Memorandum

TO: $\quad$ Thomas Davy, P.E., City of Henderson
DATE: November 27, 2019
FROM: John Karachepone, P.E., Jacobs

SUBJECT: I-515/l-215 Interchange Feasibility Study: Traffic Forecasting Memorandum
COPIES: Chris Wright, NDOT; Mark Wooster, NDOT; Hoang Hong, P.E., NDOT; Samuel Ahiamadi, NDOT; David Bowers, P.E., NDOT; Jim Mischler, P.E., CA Group

## 1. INTRODUCTION AND BACKGROUND

The I-515/l-215 Interchange Feasibility Study was initiated by the City of Henderson to develop and evaluate alternatives to alleviate recurring congestion, address high crash locations, and to accommodate future growth at the interchange and adjoining interstate corridors.

In 2015, the City initiated the Southbound I-515 Improvement Study to assess deteriorating traffic operations, including low travel speeds and long queues, on the interstate system-to-system ramp from I-515 southbound (SB) to I-215 westbound (WB). The results of the study included a shortterm recommendation to reconfigure the I-515 SB to I-215 WB ramp. NDOT, in turn, has designed and implemented this short-term solution in December 2018.

In 2016, NDOT initiated the Southern Nevada Traffic Study (SNTS) to understand the existing and future freeway operations and to develop improvement concepts for poorly performing freeway segments in Southern Nevada. As part of the SNTS, the I-515/I-215 interchange was modeled at a microscopic simulation level of detail using Aimsun Next and evaluated for various improvement concepts to improve traffic operations.

This feasibility study builds upon and advances the findings and recommendations of the previous studies. This study is designed to identify long-term solutions to advance under the direction of the City and NDOT into the NEPA process, and subsequently into final design and construction. One of the key steps in the feasibility study is the evaluation of the traffic operations performance of improvement alternatives.

The Project team originally intended to use the Aimsun Next model developed, calibrated, and utilized by the SNTS, without any modifications to model the year 2017 Existing Conditions and
year 2040 No-Action Alternative. This proposed methodology was documented in the January 28, 2019 memorandum": "I-515/l-215 Interchange Feasibility Study: Traffic Operations Methodology Memorandum," included as Appendix A. However, during the Project, discrepancies were observed between the year 2017 Aimsun Next model volumes and the corresponding NDOT field counts. Similarly, the model's year 2040 volumes were noted to be of concern because the future year volumes did not have a reasonable growth over year 2017 volumes. These observations were documented in the May 6, 2019 memorandum: "I-515/l-215 Interchange Feasibility Study: Aimsun Next Model Observations."

Due to these concerns, the Project team decided to update the calibration of the "I-515/I-215 FS" subarea (the study area of this Feasibility Study) to improve the model's ability to reflect Existing Conditions (the year 2017) volumes and consequently, to improve the reliability of the model's year 2040 forecast volumes and operational results. Therefore, the Project team completed static and dynamic calibration of the l-515/l-215 FS subarea. Where possible, the Project team retained the assumptions and parameters of the previous modeling effort completed as part of SNTS. This memorandum summarizes the calibration methodology, assumptions, and results. Subsequently, the Project team utilized the calibrated model to develop the future year 2040 traffic volumes. This memorandum also documents the methodology and assumptions involved with the process of developing the future year volumes. Appendix B of this memorandum contains the electronic files for the Aimsun Next model. A completed "Traffic Forecasting Guidelines Checklist" is included in Appendix C.

## 2. PROJECT LIMITS

The I-515/I-215 Interchange lies in the heart of the City of Henderson, Nevada. The Project limits for Aimsun Next modeling and traffic operations analysis include:

- I-515 Freeway between (and including) Sunset Road to the north and Horizon Drive to the south. The Galleria Drive on-ramp to I-515 SB and the Galleria Drive off-ramp from I-515 northbound (NB) are also included.
- I-215 Freeway/Lake Mead Parkway between (and including) Stephanie Street to the west and Eastgate Road to the east. The Valle Verde Drive on-ramp to l-215 eastbound (EB) and the Valle Verde Drive off-ramp from I-215 WB are also included.

[^0]Figure 1 shows the Project limits for the operations analysis. The following are the study intersections included in the analysis:

1. I-515 NB and Sunset Road
2. I-515 SB and Sunset Road
3. I-515 NB and Auto Show Drive
4. I-515 SB and Auto Show Drive
5. I-515 NB and Horizon Drive
6. I-515 SB and Horizon Drive
7. I-215 EB and Stephanie Street
8. I-215 WB and Stephanie Street
9. I-215 EB and Gibson Road
10. I-215 WB and Gibson Road
11. Gibson Road and Wigwam Parkway
12. Gibson Road and Las Palmas Entrada Avenue
13. Lake Mead Parkway and Eastgate Road
14. Auto Show Drive and Eastgate Road

Figure 1: Project Limits for Traffic Operations Analysis


## 3. TECHNICAL GUIDANCE, STANDARDS, AND TOOLS

The following technical documents and guidelines are the key references that were used in the traffic analysis and modeling of this study:

- Aimsun Next Modeling Guidelines, NDOT, 2018
- Technical memorandums developed, reviewed, and approved (by NDOT) for this Project:
- I-515/l-215 Interchange Feasibility Study: Traffic Operations Methodology Memorandum, January 2019
- I-515/l-215 Interchange Feasibility Study: Aimsun Next Model Observations, May 2019
- Traffic Forecasting Methods and Assumptions Memorandum (Appendix A of NDOT SNTS Final Report), 2018
- Traffic Operations Methodology and Assumptions Memorandum (Appendix B of NDOT SNTS Final Report), 2018
- 2017 Aimsun Next Model Development and Calibration Report (Appendix C of NDOT SNTS Final Report), 2018
- Existing Conditions Report (Appendix D of NDOT SNTS Final Report), 2018
- Future Conditions Report (Appendix E of NDOT SNTS Final Report), 2018
- Highway Capacity Manual 6 ${ }^{\text {th }}$ Edition, Transportation Research Board, 2016

Traffic modeling was completed using Aimsun Next (Version 8.2.4).

## 4. YEAR 2017 STATIC VOLUME CALIBRATION AND DEVELOPMENT OF TRAFFIC DEMAND

### 4.1. Development of the Year 2017 Aimsun Next Model

Modeling for this Project was completed using the Southern Nevada Aimsun Next model provided by NDOT. The I-515/l-215 interchange was previously modeled during SNTS; the "I-215/l-515" subarea in the Southern Nevada Aimsun Next model was developed as part of SNTS. This subarea (the year 2017 for existing conditions) was modeled to a microscopic level of detail as part of SNTS. Where needed, the existing conditions network coding was augmented for this Project. As an example, the intersections of Gibson Road/Wigwam Parkway and Gibson Road/Las Palmas Entrada Avenue were not modeled to a microscopic level of detail as part of SNTS. Therefore, the geometry and the existing signal timings for these intersections were modeled as part of this Project. The Southern Nevada Aimsun Next model includes a two-hour

AM peak (7:00 AM - 9:00 AM) and PM peak (4:00 PM - 6:00 PM) period origin-destination (OD) matrices for the I-215/l-515 subarea. The modeling periods for this Project matches these periods.

### 4.2. Creation of Subnetwork and Static Traversal

For this Project, NDOT created a new subarea, the "I-515/l-215 FS" subarea in the Southern Nevada Aimsun Next model. This new subarea focuses on the freeway sections and intersections listed in Section 2 and shown in Figure 1. All modeling for this Project was completed within this new I-515/l-215 FS subarea.

The static traversal procedure for the l-515/l-215 FS subarea was run using the year 2017 static assignment results of the SNTS' I-215/l-515 subarea to extract demands/Origin-Destination (OD) matrices for the $\mathrm{I}-515 / \mathrm{l}-215 \mathrm{FS}$ subarea for the AM and the PM period under existing conditions. The static traversal procedure produced the following four OD matrices for each modeling period:

- Drive Alone (DA)
- Shared Ride 2 passengers per vehicle (SR2)
- $\quad$ Shared Ride 3 or more passengers per vehicle (SR3)
- Truck

Similarly, for the future year 2040, the static traversal procedure for the I-515/l-215 FS subarea was run using the year 2040 Build Alternative's static assignment results of the SNTS' I-215/I-515 subarea to extract the year 2040 demands/OD matrices for the AM and the PM period for the I-515/l-215 FS subarea. These OD matrices (the year 2040) were later used in the development of future year volumes (see Section 6.2).

### 4.3. Year 2017 Static Volume Calibration

The year 2017 volumes for the freeway mainline and ramps were available and obtained from NDOT's short-term count stations. These NDOT counts were observed in the field during June and September. Within the Project limits, March was identified to be a month of peak traffic (based on NDOT ATR \#0035370 [IR215 .5 mi W of Gibson Intch]). Therefore, the raw NDOT counts were seasonally adjusted using the factors from ATR \#0035370 before using them in static calibration.

The seasonally adjusted count data (7:00 AM - 9:00 AM and 4:00 PM - 6:00 PM) were compiled at both a 15-minute aggregation interval and a two-hour interval and used for OD matrix adjustment in the model. The static traversal procedure explained in the previous Section produced two-hour (7:00 AM - 9:00 AM and 4:00 PM - 6:00 PM) OD matrices for the "I-515/I-215 FS" subarea.

A Static OD Adjustment Experiment was first run to adjust the two-hour OD matrices using the two-hour field count data. The resultant adjusted two-hour OD matrices were then used as input to a Static OD Departure Adjustment Experiment; the 15-minute field count data was used as the basis for this adjustment experiment. This Departure Adjustment Experiment produced 15-minute OD matrices, thus imparting a time-varying "profile" to the demand. These steps were repeated once for the AM period and again for the PM period. At the end of this process, the refined OD matrices produced freeway mainline and ramp volumes in the model that resembled the field counts. Section 5.1 shows the volume calibration targets and Section 5.3 shows the results of the calibration.

## 5. YEAR 2017 DYNAMIC CALIBRATION

The refined OD matrices (obtained as explained in Section 4.3) were used to run the year 2017 dynamic microsimulation scenarios. The existing traffic signal timing and ramp meter timing information included in the Southern Nevada Aimsun Next model were used for the year 2017 existing conditions model. The Southern Nevada Aimsun Next model did not include signal timing information for the intersections of Gibson Road/Wigwam Parkway and Gibson Road/Las Palmas Entrada Avenue. Existing traffic signal timing for these intersections was obtained from RTC FAST and coded in the model.

### 5.1. Calibration Measures of Effectiveness (MOEs) and Targets

In addition to volume calibration, spot speeds along the freeways was selected as the MOE for calibration. Calibration targets for these MOEs are listed in Table 1.

Table 1: Calibration Targets for an Acceptable Match

| Calibration <br> MOE | Calibration Criteria and Measures | Calibration Target |
| :---: | :---: | :---: | :---: | | Calibration Target adapted from Reference |
| :---: |
| Technical Guidance Document |

### 5.2. Modified Calibration Parameters

The calibration process was iterative and involved comparing model outputs with the field MOE, and then adjusting calibration parameters until an acceptable match was achieved. Several calibration parameters were adjusted to meet the calibration targets for the selected MOEs (volumes and speeds), and to match the observed field conditions. As a first step, the Distance Zone 1 and Distance Zone 2 values for freeway off-ramps were set to 5,000 feet and 2,500 feet respectively to better reflect the location of exit information signs and driver behavior in the field. Similarly, the Side Lane Merging Distance for freeway on-ramps was set to 1,000 feet to better model the merging behavior. Table 2 and Table 3 list the adjustments to the calibration parameters made to the model, the specific location of these adjustments, and the rationale behind the adjustments for the AM period and the PM period respectively. The modified calibration parameters are stored as Attribute Overrides in the Aimsun Next model.

Table 2: Modified Calibration Parameters - AM Period

| No. | Location | Aimsun Next Object | Calibration Parameter | New Value | Rationale |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $1-215 \mathrm{~EB} /$ Stephanie Street off-ramp | 356205: RAMP I215 E STEPHANI <br> (20212) - Section | Acceleration Factor | 2 | With the default model parameters, long queues were observed in the model at this off-ramp/ramp terminal intersection and vehicles spilled back onto the freeway. This limited the number of vehicles that could travel past this point and created traffic flow issues downstream of here. Therefore, these model parameters were modified to increase the aggressiveness of vehicles in the model. With these changes, the queues at the off-ramp/ramp terminal intersection better match field conditions. |
| 2 |  | 5947: RAMP I215 E STEPHANI (20212) - Section | Acceleration Factor | 2 |  |
| 3 |  | 356207: RAMP I215 E STEPHANI (20212) - Section | Acceleration Factor | 2 |  |
| 4 | I-215 WB between Gibson Road and Stephanie Street | 11197: \| 215 (22253) - Section | Deceleration Factor | 4 | Vehicles were observed to travel at higher speeds in the model than what was observed in the field along this stretch of the freeway when the default model parameters were used. Therefore, these model parameters were modified to better reflect the congested conditions observed in the field. |
| 5 |  | 11197: I 215 (22253) - Section | Lane-Changing Cooperation | 0 |  |
| 6 | I-215 WB/Stephanie Street off-ramp | 47271 - Turn | Distance Zone 1 | 1000 |  |
| 7 |  | 47271 - Turn | Distance Zone 2 | 500 |  |
| 8 | I-515 NB downstream of the Horizon Drive on-ramp | 6177: US 95 (9605) - Section | Acceleration Factor | 2 | With the default model parameters, unreasonably long queues were observed in the model, upstream of the on-ramp merge and spilling back along Horizon Drive. This also limited the number of vehicles processed through this on-ramp onto the freeway. Therefore, these model parameters were modified to increase the aggressiveness of vehicles in the model. With these changes, the operations of the ramp and the merge segment better match field conditions. |
| 9 |  | 6177: US 95 (9605) - Section | Imprudent Lane Changing | TRUE |  |
| 10 | I-515 NB between I-215 EB on-ramp and Auto Show Drive on-ramp | 17600: US 95 (36462) - Section | Imprudent Lane Changing | TRUE | With the default model parameter, vehicles in the model were observed to be more conservative than in the field when completing the merge/lane-change maneuver. Therefore, this model parameter was modified to better reflect the driving behavior observed in the field. |

Table 3: Modified Calibration Parameters - PM Period


Table 3: Modified Calibration Parameters - PM Period (continued)

| No. | Location | Aimsun Next Object | Calibration Parameter | New Value | Rationale |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | I-215 EB to I-515 NB ramp | 27970 - Turn | Distance Zone 1 | 10000 |  |
| 16 |  | 27970 - Turn | Distance Zone 2 | 6500 | parameters were modified to better match the lane positioning and driving behavior observed in |
| 17 | I-215 EB to I-515 SB ramp | 27969 - Turn | Distance Zone 1 | 10000 | upstream of this location. |
| 18 |  | 27969 - Turn | Distance Zone 2 | 6500 |  |
| 19 | I-215 EB to I-515 SB ramp | 6193: RAMP EI 215 US95 S <br> (32348) - Section | Lane-Changing Aggressiveness | 50 |  |
| 20 | 1-515 SB downstream of the l-215 EB on-ramp | 6170: US 95 (9451) - Section | Lane-Changing Aggressiveness | 50 |  |
| 21 |  | 6176: US 95 (9671) - Section | Lane-Changing Aggressiveness | 50 | the field when completing the merge/lane-change maneuver. Therefore, these model parameters were |
| 22 | I-515 NB between I-215 EB on-ramp and Auto Show Drive on-ramp | 17600: US 95 (36462) - Section | Lane-Changing Aggressiveness | 80 |  |
| 23 |  | 17600: US 95 (36462) - Section | Imprudent Lane Changing | true |  |

### 5.3. Volume Calibration

A comparison of the microsimulation model traffic flows to field count volumes is shown in Table 4 and Table 5 for the AM and the PM period respectively. Graphical results of volume calibration are shown in Figure 2 and Figure 3 for the AM period, and Figure 4 and Figure 5 for the PM period. A detailed comparison of the model traffic flows to field count volumes is provided in Appendix D.

The results show that all calibration targets are met for the AM period except for one location during the 7:00 AM to 8:00 AM period, where the model volume was higher than the field volume. At this location, the model volume was approximately 311 vehicles more than field observed volume (exceeded the $250 \mathrm{veh} / \mathrm{h}$ target). Similarly, the results show that all calibration targets are met for the PM period except for one location during the 4:00 PM to 5:00 PM period, where the model volume was higher than the field volume. At this location, the model volume was approximately 251 vehicles more than field observed volume (exceeded the 250 veh/h target by one veh $/ \mathrm{h}$ ). In both these cases, the targets were exceeded only slightly and the calculated GEH is less than 4.0. Furthermore, from Figure 2 through Figure 5, it can be seen that there is a good overall fit between the field and the model volumes. Therefore, the model volumes are considered calibrated.

Table 4: Link/Section Volume Calibration Results - AM Period

| Criteria | Acceptance Target | 7AM |  |  | 8AM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Points | Pass | Acceptance | Points | Pass | Acceptance |
| FLOW < 700, within 100 veh/h | > 85\% | 17 | 17 | 100.0 | 20 | 20 | 100.0 |
| 700 < FLOW < 2700, within 15\% | > 85\% | 13 | 13 | 100.0 | 10 | 10 | 100.0 |
| 2700 < FLOW < 5000, within $10 \%$ | > 85\% | 2 | 2 | 100.0 | 3 | 3 | 100.0 |
| FLOW > 5000 within 250 veh/h | > 85\% | 3 | 2 | 66.7 | 2 | 2 | 100.0 |
| GEH Statistic < 5 for individual link flows | > 85\% | 35 | 35 | 100.0 | 35 | 35 | 100.0 |
| GEH Statistic < 10 for individual link flows | 100\% | 35 | 35 | 100.0 | 35 | 35 | 100.0 |
| Sum of all link flows | > 95\% |  |  | 97.7 |  |  | 99.9 |

Table 5: Link/Section Volume Calibration Results - PM Period

| Criteria | Acceptance Target | 4PM |  |  | 5PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Points | Pass | Acceptance | Points | Pass | Acceptance |
| FLOW < 700, within 100 veh/h | > 85\% | 14 | 14 | 100.0 | 14 | 14 | 100.0 |
| 700 < FLOW < 2700, within 15\% | > 85\% | 18 | 18 | 100.0 | 18 | 18 | 100.0 |
| 2700 < FLOW < 5000, within $10 \%$ | > 85\% | 2 | 2 | 100.0 | 2 | 2 | 100.0 |
| FLOW > 5000 within 250 veh/h | > 85\% | 2 | 1 | 50.0 | 2 | 2 | 100.0 |
| GEH Statistic < 5 for individual link flows | > 85\% | 36 | 34 | 94.4 | 36 | 36 | 100.0 |
| GEH Statistic < 10 for individual link flows | 100\% | 36 | 36 | 100.0 | 36 | 36 | 100.0 |
| Sum of all link flows | > 95\% |  |  | 97.9 |  |  | 99.9 |

Figure 2: Link/Section Volume Calibration (Graphical) Results for 7:00 AM to 8:00 AM


INTERCHANGE
Figure 3: Link/Section Volume Calibration (Graphical) Results for 8:00 AM to 9:00 AM


Figure 4: Link/Section Volume Calibration (Graphical) Results for 4:00 PM to 5:00 PM


Figure 5: Link/Section Volume Calibration (Graphical) Results for 5:00 PM to 6:00 PM


### 5.4. Speed Calibration

Field spot speed data along the freeways were available from SNTS. Spot speed data was available for the entire modeling period (AM and PM) at four locations within the Project limits. These locations are:

- I-215 EB east of Stephanie Street
- Lake Mead Parkway (I-215 WB) east of I-515
- I-215 WB east of Stephanie Street
- I-515 NB north of Horizon Drive

Detectors were placed in the Aimsun Next model, and the speed data from these detectors in the model were compared to the field spot speed data for calibration.

Table 6 and Table 7 show the spot speed calibration results for the AM and the PM period respectively; Figure 6 through Figure 9 and Figure 10 through Figure 13 show the field and model speeds in graphical form for the AM and the PM period respectively. Table 6 and Table 7 show the field speed data, speeds observed in the model (detectors), the percent difference and the absolute difference in the speeds. Initially, the posted speed limit ( 65 mph ) was used as the Maximum Speed in the Aimsun Next model for all freeway sections. However, the field observed spot speed data shows that at some locations within the Project limits, the observed speed is higher than the posted speed limit. When the model was run with the posted speed limit as the Maximum Speed, the simulated speed observed at model detectors did not match the field spot speed. Therefore, the Maximum Speed was increased to 70 mph to better model field conditions.

As seen from Table 6, the speed calibration targets are met (for each 15-minute period) at three out of four locations in the AM period. Similarly, from Table 7, the speed calibration targets are met (for each 15-minute period) at three out of four locations in the PM period. At these locations, the absolute difference in speeds is usually within 5 mph , much less than the target of 10 mph . The calibration target is not met (for each 15-minute period) at I-215 WB east of Stephanie Street in the AM period and I-215 EB east of Stephanie Street in the PM period. In both these cases, it is noted that the absolute difference in speeds for the entire two-hour period is within the target of 10 mph . The field spot speed data was obtained from NDOT's SNTS, which was collected in early 2017. The volume/count data was collected in 2017 and seasonally adjusted to March 2017 (as explained in Section 4.3). After multiple iterations, with various changes to the model parameters, the speed calibration target was not met at both these locations. The speed calibration target is likely not met because the volume and speed data were collected during different periods, representing different traffic flow/peaking patterns. Unrealistic changes to the
model would likely be needed to meet the targets at these two locations; therefore, it was decided to leave the targets unmet at these locations. However, from Figure 8 and Figure 10, it can be seen that the severity of the congestion at these locations is replicated in the model (although during a different 15 -minute period).

Table 6: Speed Calibration Results - AM Period

|  | Field Observed Speeds (mph) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | I-215 EB east of Stephanie <br> Street | Lake Mead Parkway <br> (I-215 WB) east of I-515 | I-215 WB east of <br> Stephanie Street | I-515 NB north of Horizon <br> Drive |
| 7:00 to 7:15 AM | 65.4 | 53.7 | 60.6 | 65.8 |
| 7:15 to 7:30 AM | 65.1 | 51.2 | 50.9 | 64.8 |
| 7:30 to 7:45 AM | 64.6 | 49.0 | 34.7 | 64.7 |
| 7:45 to 8:00 AM | 64.6 | 45.9 | 29.5 | 66.6 |
| 8:00 to 8:15 AM | 64.6 | 47.3 | 44.9 | 65.1 |
| 8:15 to 8:30 AM | 64.5 | 45.6 | 54.0 | 65.7 |
| 8:30 to 8:45 AM | 65.1 | 49.5 | 52.9 | 66.2 |
| 8:45 to 9:00 $\mathbf{~ A M ~}$ | 64.0 | 49.1 | 51.7 | 65.4 |
| $\mathbf{7 : 0 0}$ to 9:00 $\mathbf{~ M M ~}$ | 64.7 | 48.9 | 47.4 | 65.5 |


|  | Aimsun Next Model Speeds (mph) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | I-215 EB east of Stephanie <br> Street | Lake Mead Parkway <br> (I-215 WB) east of I-515 | I-215 WB east of <br> Stephanie Street | I-515 NB north of Horizon <br> Drive |
| 7:00 to 7:15 AM | 67.7 | 49.6 | 27.0 | 64.9 |
| 7:15 to 7:30 AM | 66.6 | 50.2 | 39.8 | 64.7 |
| 7:30 to 7:45 AM | 65.5 | 49.0 | 62.3 | 67.0 |
| 7:45 to 8:00 AM | 65.3 | 48.8 | 60.3 | 67.8 |
| 8:00 to 8:15 AM | 67.5 | 50.0 | 62.4 | 68.5 |
| 8:15 to 8:30 AM | 67.5 | 49.2 | 58.7 | 68.1 |
| 8:30 to 8:45 AM | 67.4 | 50.7 | 60.8 | 68.1 |
| 8:45 to 9:00 AM | 67.2 | 50.4 | 62.4 | 67.8 |
| 7:00 to 9:00 AM | 66.7 | 49.7 | 53.3 | 67.0 |


|  | Percent Difference between Field Observed Speeds and Aimsun Next Model Speeds |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | I-215 EB east of Stephanie Street | Lake Mead Parkway (I-215 WB) east of I-515 | I-215 WB east of Stephanie Street | I-515 NB north of Horizon Drive |
| 7:00 to 7:15 AM | -4\% | 8\% | 55\% | 1\% |
| 7:15 to 7:30 AM | -2\% | 2\% | 22\% | 0\% |
| 7:30 to 7:45 AM | -1\% | 0\% | -80\% | -4\% |
| 7:45 to 8:00 AM | -1\% | -6\% | -104\% | -2\% |
| 8:00 to 8:15 AM | -5\% | -6\% | -39\% | -5\% |
| 8:15 to 8:30 AM | -5\% | -8\% | -9\% | -4\% |
| 8:30 to 8:45 AM | -4\% | -3\% | -15\% | -3\% |
| 8:45 to 9:00 AM | -5\% | -3\% | -21\% | -4\% |
| 7:00 to 9:00 AM | -3\% | -1\% | -12\% | -2\% |


|  | Absolute Difference between Field Observed Speeds and Aimsun Next Model Speeds (mph) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | I-215 EB east of Stephanie Street | Lake Mead Parkway ( $\mathrm{I}-215 \mathrm{WB}$ ) east of I-515 | I-215 WB east of Stephanie Street | I-515 NB north of Horizon Drive |
| 7:00 to 7:15 AM | 2.3 | 4.2 | 33.6 | 0.9 |
| 7:15 to 7:30 AM | 1.5 | 1.0 | 11.1 | 0.1 |
| 7:30 to 7:45 AM | 0.9 | 0.0 | 27.6 | 2.3 |
| 7:45 to 8:00 AM | 0.8 | 2.9 | 30.7 | 1.1 |
| 8:00 to 8:15 AM | 2.9 | 2.7 | 17.5 | 3.4 |
| 8:15 to 8:30 AM | 3.0 | 3.5 | 4.7 | 2.3 |
| 8:30 to 8:45 AM | 2.3 | 1.3 | 8.0 | 1.9 |
| 8:45 to 9:00 AM | 3.1 | 1.2 | 10.7 | 2.4 |
| 7:00 to 9:00 AM | 2.0 | 0.7 | 5.9 | 1.4 |

Table 7: Speed Calibration Results - PM Period

|  | Field Observed Speeds (mph) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | I-215 EB east of Stephanie <br> Street | Lake Mead Parkway <br> (I-215 WB) east of I-515 | I-215 WB east of <br> Stephanie Street | I-515 NB north of Horizon <br> Drive |
| 4:00 to 4:15 PM | 48.7 | 47.2 | 56.9 | 63.9 |
| 4:15 to 4:30 PM | 53.0 | 48.8 | 52.5 | 63.4 |
| 4:30 to 4:45 PM | 58.7 | 52.3 | 54.6 | 64.5 |
| 4:45 to 5:00 PM | 58.9 | 49.4 | 57.5 | 63.7 |
| 5:00 to 5:15 PM | 54.7 | 48.1 | 60.7 | 64.9 |
| 5:15 to 5:30 PM | 51.1 | 47.0 | 58.0 | 64.2 |
| 5:30 to 5:45 PM | 52.3 | 47.3 | 56.2 | 63.3 |
| 5:45 to $\mathbf{6 : 0 0 ~ P M ~}$ | 51.8 | 49.9 | 59.5 | 63.8 |
| 4:00 to 6:00 PM | 53.6 | 48.7 | 57.0 | 64.0 |


|  | Aimsun Next Model Speeds (mph) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | I-215 EB east of Stephanie <br> Street | Lake Mead Parkway <br> (I-215 WB) east of I-515 | I-215 WB east of <br> Stephanie Street | I-515 NB north of Horizon <br> Drive |
| 4:00 to 4:15 PM | 56.1 | 48.2 | 62.6 | 65.4 |
| 4:15 to 4:30 PM | 41.2 | 48.5 | 62.3 | 66.8 |
| 4:30 to 4:45 PM | 48.5 | 48.4 | 63.0 | 65.9 |
| 4:45 to 5:00 PM | 40.4 | 49.6 | 64.2 | 66.8 |
| 5:00 to 5:15 PM | 52.6 | 48.4 | 63.1 | 65.7 |
| 5:15 to 5:30 PM | 43.7 | 49.8 | 64.9 | 66.2 |
| 5:30 to 5:45 PM | 44.9 | 49.2 | 64.6 | 67.1 |
| 5:45 to 6:00 PM | 52.0 | 50.3 | 65.7 | 67.0 |
| 4:00 to 6:00 PM | 47.5 | 48.9 | 63.7 | 66.3 |


|  | Percent Difference between Field Observed Speeds and Aimsun Next Model Speeds |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | I-215 EB east of Stephanie <br> Street | Lake Mead Parkway <br> (I-215 WB) east of I-515 | I-215 WB east of <br> Stephanie Street | I-515 NB north of Horizon <br> Drive |
| 4:00 to 4:15 PM | $-15 \%$ | $-2 \%$ | $-10 \%$ | $-2 \%$ |
| 4:15 to 4:30 PM | $22 \%$ | $1 \%$ | $-19 \%$ | $-5 \%$ |
| 4:30 to 4:45 PM | $17 \%$ | $8 \%$ | $-15 \%$ | $-2 \%$ |
| 4:45 to 5:00 PM | $31 \%$ | $0 \%$ | $-12 \%$ | $-5 \%$ |
| 5:00 to 5:15 PM | $4 \%$ | $-1 \%$ | $-4 \%$ | $-1 \%$ |
| 5:15 to 5:30 PM | $15 \%$ | $-6 \%$ | $-12 \%$ | $-3 \%$ |
| 5:30 to 5:45 PM | $14 \%$ | $-4 \%$ | $-15 \%$ | $-6 \%$ |
| 5:45 to 6:00 PM | $0 \%$ | $-1 \%$ | $-10 \%$ | $-5 \%$ |
| 4:00 to 6:00 PM | $11 \%$ | $0 \%$ | $-12 \%$ | $-4 \%$ |


|  | Absolute Difference between Field Observed Speeds and Aimsun Next Model Speeds (mph) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| I-215 EB east of Stephanie <br> Street | Lake Mead Parkway <br> (I-215 WB) east of I-515 | I-215 WB east of <br> Stephanie Street | I-515 NB north of Horizon <br> Drive |  |
| 4:00 to 4:15 PM | 7.5 | 1.0 | 5.7 | 1.5 |
| 4:15 to 4:30 PM | 11.8 | 0.3 | 9.7 | 3.4 |
| 4:30 to 4:45 PM | 10.1 | 4.0 | 8.4 | 1.4 |
| 4:45 to 5:00 PM | 18.5 | 0.2 | 6.7 | 3.1 |
| 5:00 to 5:15 PM | 2.2 | 0.3 | 2.4 | 0.8 |
| 5:15 to 5:30 PM | 7.4 | 2.8 | 6.9 | 1.9 |
| 5:30 to 5:45 PM | 7.3 | 1.9 | 8.4 | 3.8 |
| 5:45 to 6:00 PM | 0.2 | 0.4 | 6.1 | 3.1 |
| 4:00 to 6:00 PM | 6.2 | 0.2 | 6.7 | 2.4 |

Figure 6: Comparison of Field Observed and Model Speeds - AM Period - I-215 EB east of Stephanie Street


Figure 7: Comparison of Field Observed and Model Speeds - AM Period - Lake Mead Parkway (I-215 WB) east of I-515


Figure 8: Comparison of Field Observed and Model Speeds - AM Period - I-215 WB east of Stephanie Street


Figure 9: Comparison of Field Observed and Model Speeds - AM Period - I-515 NB north of Horizon Drive


Figure 10: Comparison of Field Observed and Model Speeds - PM Period - I-215 EB east of Stephanie Street


Figure 11: Comparison of Field Observed and Model Speeds - PM Period - Lake Mead Parkway (I-215 WB) east of I-515


Figure 12: Comparison of Field Observed and Model Speeds - PM Period - I-215 WB east of Stephanie Street


Figure 13: Comparison of Field Observed and Model Speeds - PM Period - I-515 NB north of Horizon Drive


## 6. FUTURE YEAR 2040 TRAFFIC FORECASTS

### 6.1. Forecast Scenarios

Peak hour volume forecasts were developed for the following forecast scenarios:

- Future Year 2040 No-Action Alternative
- Future Year 2040 Build Alternatives (Two options)

Within this Project's limits, the year 2040 No-Action Alternative network included the changes introduced as part of the I-515/l-215 Restriping Project. NDOT implemented the I-515/l-215 Restriping Project during the second half of 2018; therefore, this was not part of the existing conditions year 2017 network. The schematics for the two Build Alternative options that were modeled are included in Appendix E.

### 6.2. Future Year 2040 Peak Hour Volumes

The year 2040 No-Action Alternative and Build Alternative (microsimulation level-of-detail) networks were modeled in Aimsun Next, and the changes to calibration parameters (from the base year 2017 model - shown in Table 2 and Table 3) were replicated in these future year networks. Changes corresponding to the future year network were coded as Geometry Configurations in Aimsun Next; changes to the roadway network were made only within this Project's limits. No changes were made to the Aimsun Next roadway network outside of this Project's limits.

The following series of steps were completed to develop the year 2040 No-Action Alternative and Build Alternative scenarios in the Aimsun Next model. These steps were repeated twice, once for the AM modeling period and again for the PM period:

1. The year 2017 OD matrices for the I-515/I-215 FS subarea were refined as part of static calibration (explained in Section 4.3).
a. The adjustments made to the year 2017 OD matrices as part of calibration were replicated in the year 2040 OD matrices. ${ }^{2}$
b. This was accomplished using the "Pivot-Point Method" utilized in NDOT SNTS. Additional details of this methodology are available in the 2040 Micro/Meso Future Volume Development Technical Memorandum (Appendix F). The adjusted OD

[^1]matrices corresponding to the I-515/l-215 FS subarea were used for all further modeling steps.
2. The time-varying "profile" of the year 2017 traffic demand was applied to the year 2040 demand. With this, traffic demands were available for the two-hour modeling period with a time-varying "profile," with the demand varying every 15 minutes.
3. The macroscopic static assignment was run using this two-hour demand (with a timevarying profile) for the I-515/l-215 FS subarea for the No-Action Alternative and the Build Alternatives to develop the year 2040 static assigned volumes and to generate a path assignment for dynamic microsimulation.
4. For documentation, a peak one-hour (7:30 AM to 8:30 AM for the AM period and 4:30 PM to $5: 30 \mathrm{PM}$ for the PM period) demand was also created. The macroscopic static assignment was run using this peak hour demand to develop the year 2040 peak hour static assigned volumes. These year 2040 peak hour volumes are shown in Figure 14 through Figure 16 and are the traffic forecasts for the Project.
HENDERSON
INTERCHANGE

Figure 14: Year 2040 No-Action Alternative Peak Hour Volumes (along I-215)

| AM Demand Volume (vph) | 7610 | 450 | 8060 | 1300 | 6760 | 1040 | 7800 | 1200 | 6600 | 810 | 7410 | 2690 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PM Demand Volume (vph) | 7770 | 740 | 8510 | 2040 | 6470 | 830 | 7300 | 1070 | 6230 | 860 | 7090 | 2100 |








## Figure 16: Year 2040 Build Alternative Option 2 Peak Hour Volumes (along I-515)

| AM Demand Volume (vph) | 7240 | 1050 | 6190 | 370 | 6560 | 1000 | 7560 | 540 | 7020 | 1450 | 5570 | 390 | 5960 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PM Demand Volume (vph) | 5940 | 910 | 5030 | 780 | 5810 | 1130 | 6940 | 800 | 6140 | 1230 | 4910 | 610 | 5520 |
|  |  | from Sunset | to Galleria |  | Sunset |  |  |  |  |  |  |  |  |



### 6.3. AADT and Heavy Vehicles Forecast

AADT forecasts were developed for the year 2040 No-Action Alternative and the Build Alternative options, using the peak hour volumes presented in Figure 14 through Figure 16. A $\mathrm{K}_{30}$ of 8.4 percent (from NDOT ATR \#0032230 [IR515/US95 . 3 mi S of Russell Rd]) was used to determine the AADT. The AADT forecasts are presented in Appendix G.

The heavy vehicles percentage for future year conditions for the Project was calculated based on the trips in the "Truck" OD matrices and the trips in OD matrices for all vehicle types, developed for the l-515/l-215 FS subarea. Note that the OD matrices in the Aimsun Next model for this Project were developed using the OD matrices for SNTS' l-215/l-515 subarea, which were originally developed from the RTC's regional travel demand model.

The heavy vehicles percentage for future year conditions (the year 2040 No-Action Alternative and Build Alternatives) is estimated to be 4.7 percent for the AM peak period and 7.7 percent for the PM peak period.

## 7. SUMMARY AND CONCLUSION

This memorandum summarizes the existing conditions (the year 2017) calibration methodology, assumptions, and results. This memorandum also documents the methodology and assumptions involved in the development of the future (the year 2040) traffic volumes for the I-515/I-215 Interchange Feasibility Study. NDOT review and approval of the year 2040 traffic forecasts (Section 6) is requested before using the forecast volumes and associated traffic operations results for NEPA documentation.

## Appendices

Appendix A: I-515/I-215 Interchange Feasibility Study: Traffic Operations Methodology Memorandum

Appendix B: Electronic Files of the Aimsun Next Model and other Associated Model Files
Appendix C: Traffic Forecasting Guidelines Checklist
Appendix D: Detailed Volume Calibration Results
Appendix E: Schematics of the Build Alternative Options modeled in Aimsun Next Appendix F: NDOT SNTS' 2040 Micro/Meso Future Volume Development Technical Memorandum Appendix G: Future Year 2040 AADTs INTERCHANGE

Traffic Forecasting Memorandum

## Appendices

Appendix A
I-515/I-215 Interchange Feasibility Study: Traffic Operations Methodology Memorandum

## Technical Memorandum

TO: Thomas Davy, P.E., City of Henderson DATE: January 28, 2019

FROM: John Karachepone, P.E., Jacobs

## SUBJECT: I-515/l-215 Interchange Feasibility Study: Traffic Operations Methodology Memorandum

COPIES: Hoang Hong, P.E., NDOT; Casey Sylvester, P.E., NDOT; Samuel Ahiamadi, NDOT; Chris Wright, NDOT; Mark Wooster, NDOT; Jack Sjostrom, P.E., CA Group

## 1. INTRODUCTION AND BACKGROUND

The I-515/I-215 Interchange Feasibility Study was initiated by the City of Henderson to develop and evaluate alternatives to alleviate recurring congestion, address high crash locations, and to accommodate future growth in the interchange and adjoining interstate corridors.

In 2015, the City initiated the Southbound I-515 Improvement Study to assess deteriorating traffic operations, including low travel speeds and long queues, on the interstate system-to-system ramp from I-515 southbound (SB) to I-215 westbound (WB). The results of the study included a shortterm recommendation to reconfigure the I-515 SB to I-215 WB ramp. NDOT, in turn, has designed and implemented this short-term solution in December 2018.

In 2016, NDOT initiated the Southern Nevada Traffic Study (SNTS) to understand the existing and future freeway operations and to develop improvement concepts for poorly performing freeway segments in Southern Nevada. As part of the SNTS, the I-515/I-215 interchange was modeled at a microscopic simulation level of detail using Aimsun Next and evaluated for various improvement concepts to improve traffic operations.

This feasibility study builds upon and advances the findings and recommendations of the previous studies. This study is designed to identify long-term solutions that could be feasibly advanced under the direction of the City and NDOT into the NEPA process and subsequently into final design and construction. One of the key steps in the feasibility study is the evaluation of the traffic operations performance of improvement alternatives. This memorandum explains the methodology and assumptions of the Aimsun Next modeling process to be used for the traffic
operations analysis. A completed "Methodology Memorandum Content Checklist" is included as Attachment 1 at the end of this memorandum.

## 2. PROJECT LIMITS

The I-515/I-215 Interchange lies in the heart of the City of Henderson, Nevada. The Project limits for Aimsun Next modeling and traffic operations analysis include:

- I-515 Freeway between (and including) Sunset Road in the north and Horizon Drive in the south. The Galleria Drive on-ramp to I-515 SB and the Galleria Drive off-ramp from I-515 northbound (NB) are also included.
- I-215 Freeway/Lake Mead Parkway between (and including) Stephanie Street in the west and Eastgate Road in the east. The Valle Verde Drive on-ramp to I-215 eastbound (EB) and the Valle Verde Drive off-ramp from I-215 WB are also included.

Figure 1 shows the Project limits for the operations analysis. The following are the study intersections that will be included in the analysis:

1. I-515 NB and Sunset Road
2. I-515 SB and Sunset Road
3. I-515 NB and Auto Show Drive
4. I-515 SB and Auto Show Drive
5. I-515 NB and Horizon Drive
6. I-515 SB and Horizon Drive
7. I-215 EB and Stephanie Street
8. I-215 WB and Stephanie Street
9. I-215 EB and Gibson Road
10. I-215 WB and Gibson Road
11. Gibson Road and Wigwam Parkway
12. Gibson Road and Las Palmas Entrada Avenue
13. Lake Mead Parkway and Eastgate Road
14. Auto Show Drive and Eastgate Road

Figure 1: Project Limits for Traffic Operations Analysis


## 3. TECHNICAL GUIDANCE, STANDARDS, AND TOOLS

The following technical documents and guidelines are the key references to be used in the traffic analysis and modeling of this study:

- Aimsun Next Modeling Guidelines, NDOT, 2018
- Traffic Forecasting Methods and Assumptions Memorandum (Appendix A of NDOT SNTS Final Report), 2018
- Traffic Operations Methodology and Assumptions Memorandum (Appendix B of NDOT SNTS Final Report), 2018
- 2017 Aimsun Next Model Development and Calibration Report (Appendix C of NDOT SNTS Final Report), 2018
- Existing Conditions Report (Appendix D of NDOT SNTS Final Report), 2018
- Future Conditions Report (Appendix E of NDOT SNTS Final Report), 2018
- Highway Capacity Manual 6 ${ }^{\text {th }}$ Edition, Transportation Research Board, 2016

Traffic microsimulation modeling will be completed using Aimsun Next version 8.2.4 (or the most recent version available at the start of the analysis). Traffic signal timings for the study intersections for Build Alternatives will be optimized using Synchro (version 10 or the most recent version available at the start of the analysis) and will be used in Aimsun Next as a starting point. Synchro and Highway Capacity Software (HCS version 7.7 or the most recent version available at the start of the analysis) will be used only as supporting traffic analysis tools. All final traffic operations analysis results will be reported from Aimsun Next.

## 4. ANALYSIS SCENARIOS, MODELING PERIODS, AND MULTIPLE TIME PERIODS

Aimsun Next microscopic simulation modeling will be completed for the following scenarios:

- Existing Year 2017 (No new modeling, reporting of results [for comparative analysis purposes] only as described in the Scope of Services)
- Future Year 2040 No-Action Alternative (No new modeling, reporting of results [for comparative analysis purposes] only as described in the Scope of Services)
- Future Year 2040 Build Alternatives (Up to three Alternatives)

The Aimsun Next scenarios for this Project will be developed using the Southern Nevada Aimsun Next model provided by NDOT. This model includes a new "I-515/l-215 FS" subarea created for this Project. The I-515/I-215 interchange was modeled during SNTS; the "I-215/I-515" subarea in the Southern Nevada Aimsun Next model was developed as part of SNTS. Along I-215, the limits
of the SNTS I-215/I-515 subarea extend from Windmill Lane to the I-515/l-215 interchange; along I-515, the limits of this subarea extend from Boulder Highway to the I-515/I-215 interchange. This subarea was modeled and calibrated to a microscopic level of detail as part of SNTS. Therefore, no new existing conditions modeling or calibration to existing conditions will be completed for this Project. Similarly, the year 2040 No-Action Alternative was modeled during SNTS; no new modeling will be completed as part of this Project for the year 2040 No-Action Alternative. However, the existing year 2017 and year 2040 No-Action Alternative microsimulation scenarios will be run in Aimsun Next for the l-515/l-215 FS subarea and results will be reported for comparative purposes.

Up to three (3) Build Alternatives for the year 2040 will be modeled to a microsimulation level as part of this Project in the I-515/l-215 FS subarea and the results will be compared against the 2040 No-Action Alternative. The Build Alternatives will be selected from a list of potential improvements through a high-level screening process; the three highest-ranked alternatives from the screening process will be modeled in Aimsun Next.

The Southern Nevada Aimsun Next model includes two-hour AM peak (7:00 AM - 9:00 AM) and PM peak (4:00 PM - 6:00 PM) period origin-destination (OD) matrices for the I-215/l-515 subarea. The modeling periods for this Project will also match these periods. For year 2017 conditions, OD matrices are available for each 15-minute period. Therefore, the existing conditions modeling for this Project will reflect this time-varying profile in demand. Such a time-varying profile in demand is not available in the Southern Nevada Aimsun Next model for future year 2040 conditions. Therefore, for the future year 2040 modeling for this Project, the variation in traffic within the twohour modeling period will not be considered; a flat two-hour demand will be used for the future year 2040 modeling.

## 5. AIMSUN NEXT MODELING - METHODOLOGY AND ASSUMPTIONS

The modeling limits for this Project consist of a new subarea (l-515/l-215 FS subarea) within the limits of the I-215/I-515 subarea developed and calibrated as part of SNTS. This new subarea focuses on the freeway sections and intersections listed in Section 2 and shown in Figure 1. All modeling for this Project will be completed within this new I-515/l-215 FS subarea created in the Southern Nevada Aimsun Next model.

The following are assumptions and key steps to be completed during the Aimsun Next modeling process:

1. The static traversal procedure for the I-515/l-215 FS subarea will be run using the year 2017 static assignment results of the SNTS' l-215/l-515 subarea to extract demands/OD matrices for the I-515/I-215 FS subarea under existing conditions. Because the I-215/I515 subarea was already calibrated as part of SNTS, the resulting traversal matrices for the I-515/I-215 FS subarea are also considered to be calibrated.
2. The subarea OD matrices generated from the static traversal (Step 1), will be used to develop and run Static Assignment and Dynamic scenarios for the year 2017 existing conditions.
a. The settings and parameters used for the scenarios in SNTS' I-215/l-515 subarea will be used for the scenarios in the new l-515/l-215 FS subarea.
3. The existing traffic signal timing and ramp meter timing information included in the Southern Nevada Aimsun Next model will be used for the year 2017 existing conditions modeling.
a. The Southern Nevada Aimsun Next model did not include signal timing information for the intersections of Gibson Road/Wigwam Parkway and Gibson Road/Las Palmas Entrada Avenue. Existing traffic signal timing for these intersections will be obtained from FAST and coded in the model.
4. The static traversal procedure for the l-515/l-215 FS subarea will be run using the year 2040 Build Alternative's static assignment results of the SNTS' I-215/I-515 subarea to extract year 2040 demands/OD matrices for the I-515/I-215 FS subarea.
a. These year 2040 matrices will be used as input demand for the year 2040 NoAction and Build Alternatives.
b. No TransCAD modeling will be completed for this Project.
5. The subarea OD matrices generated from the static traversal (Step 4), will be used to develop and run Static Assignment and Dynamic scenarios for the year 2040 No-Action and Build Alternatives.
a. The settings and parameters used for the scenarios in SNTS' I-215/l-515 subarea will be used for the scenarios in the new I-515/I-215 FS subarea.
6. Minor adjustments to traffic signal timings may be made for the year 2040 No-Action Alternative; these adjustments will be based on visual observations and engineering judgment.
7. Traffic signal timings for the year 2040 Build Alternatives will be optimized in Synchro and used in Aimsun Next.
8. Existing ramp meter timing information included in the Southern Nevada Aimsun Next model will be used for the year 2040 No-Action and Build Alternatives.
9. Because the year 2040 No-Action Alternative was developed and run as part of SNTS, it is assumed that the appropriate Dynamic calibration parameters are already coded for the year 2040 No-Action Alternative scenario.
10. For the year 2040 Build Alternatives, appropriate Dynamic calibration parameters will be coded based on the calibration parameter values in the year 2017 Dynamic scenario.

A summary of the data needs for Aimsun Next modeling and the sources for these are listed in Table 1.

Table 1: Data Needs for Modeling and Sources

| Data Need | Source |
| :---: | :---: |
| Year 2017 Existing Conditions field data for cursory review of the I-515/l-215 FS subarea | SNTS - Files dated January 2018 |
| Traffic signal timing for the following intersections that do not have signal timing coded in the Southern Nevada Aimsun Next model: <br> - Gibson Road and Wigwam Parkway <br> - Gibson Road and Las Palmas Entrada Avenue <br> - I-515 NB and Horizon Drive <br> - I-515 SB and Horizon Drive | SNTS, RTC FAST |
| Ramp metering control schedule file | SNTS - Files dated February 2018 |
| Volume and speed calibration spreadsheets | SNTS - Files dated June 2018 |
| Dynamic scenario/experiment settings/parameters ${ }^{1}$ | SNTS - Aimsun Next revision file dated July 2018 |
| Year 2017 Existing Conditions line diagram to report section-specific results | SNTS - Files dated July 2018 |
| Year 2040 No-Action Alternative line diagram to report section-specific results | Will be developed using the year 2017 Existing Conditions line diagram |
| Spreadsheets to report subarea-wide Measures of Effectiveness (MOEs) | SNTS - Files dated August 2018 |

[^2]
## 6. CURSORY REVIEW OF YEAR 2017 EXISTING CONDITIONS IN THE I-515/I215 FS SUBAREA

Even though the year 2017 existing conditions were calibrated to a microscopic level of detail as part of SNTS, and no additional calibration will be completed as part of this Project as explained previously, a cursory review of the year 2017 existing conditions in the I-515/l-215 FS subarea was completed. The results of this review are included in Attachment 2 of this memorandum. The field data obtained as part of SNTS was used for this review.

It is noted that one of the primary reasons for the variation (in the PM period) between the model outputs and the field data are the volumes at the Gibson Road and Las Palmas Entrada Avenue intersection. Las Palmas Entrada Avenue was not modeled as part of SNTS and did not exist in the Southern Nevada Aimsun Next model; this was added to the model subsequently by NDOT. The resulting year 2017 static assignment volumes for the I-515/I-215 FS subarea at this intersection are observed to be unreasonable. The model assigned PM peak hour southbound left turn volume is approximately $1,350 \mathrm{vph}$. The AM and PM peak hour static assignment volumes are included in Attachment 3. Given that the southbound left turn at the Gibson Road and Las Palmas Entrada Avenue intersection is a one-lane turn, the high turning movement volume in the PM period model results in unreasonable upstream queues through the l-215/Gibson Road interchange, which eventually spills back on to the freeway system as well.

Once the intersection turning movement volumes are collected from the field for this Project, the model volumes for this southbound left turn will be refined to be reasonably close to the field volumes. It is expected that this will result in model outputs that are slightly closer to the field data.

## 7. ANALYSIS RESULTS

The traffic operations analysis results for the year 2017 existing conditions and the future year 2040 No-Action and Build Alternatives will be obtained from the Aimsun Next model developed for this Project. Average results from 10 microsimulation runs (replications) were reported in SNTS. Therefore, results reported as part of this Project will also correspond to an average of 10 microsimulation runs.

Section-specific MOEs will be reported for all alternatives and include the following:

- Speed
- Density
- Flow
- Static Assigned Volumes

Subarea-wide MOEs will also be reported for all alternatives and include the following:

- Network Vehicles
- Latent Vehicles
- Latent Delay Time
- Number of Arrived Vehicles
- Number of Active Vehicles
- Total Network Delay
- Average Network Delay

These MOEs will be reported using the spreadsheets developed as part of the SNTS.

## 8. CONCLUSION

Following approval of this Methodology Memorandum, the Aimsun Next modeling will be completed. We request approval of this Traffic Operations Methodology Memorandum so that the operations analysis can begin.

## Attachment 1: Methodology Memorandum Content Checklist

| Item | Description | Check |
| :---: | :---: | :---: |
| Project Description and Background | Brief information about the project (purpose, general study area, etc.) | $\checkmark$ |
| Technical Guidance and Standards | Technical guidance and standards to be followed along with their version (HCM, MUTCD, NDOT Access Management Standards, etc.) | $\checkmark$ |
| Traffic Analysis Tools | Software to be used along with their version (CORSIM, HCS, TRAFFIX, etc.) | $\checkmark$ |
| Study Limits | Geographic limits of the analysis. This is to be consistent with the NDOT Microsimulation Modeling Guidelines. List all study intersections to be included. | $\checkmark$ |
| Analysis Years | Design, opening and interim years. | $\checkmark$ |
| Analysis Scenarios | Existing, No-Action, Build - describe build alternatives to the extent possible. | $\checkmark$ |
| Analysis Periods | Modeling periods and multiple time periods description. The use of multiple time periods should conform to NDOT Microsimulation Modeling Guidelines. | $\checkmark$ |
| Existing Conditions | Description of existing conditions and/or how existing analysis will be performed. | $\checkmark$ |
| Data Sources | List of sources of data and relevant information. | $\checkmark$ |
| Traffic Operations Analysis Calculations/Assumptions | Signal timing/phasing, i.e., whether to use optimized timing or actual timing data, peak hour factors, etc. | $\checkmark$ |
| Truck Percentages | Truck percentage to use for existing and future scenarios and their calculation/estimation. | N/A |
| Storage Length Calculation Method | How the turn bay lengths will be calculated. | N/A |
| Traffic Forecasts | General methodology for projecting traffic forecasts. Note that a separate Traffic Forecast Memorandum is needed for NDOT Traffic Information Division approval of the projected volumes per NDOT Traffic Forecasting Guidelines. Note if the Traffic Information Division approved the traffic forecasts. | $\checkmark$ |
| Aimsun Coding and Analysis Assumptions | Documentation of support tools (if to be used) for intersection timing/optimization (such as Synchro, TRANSYT-7F, TEAPAC etc), pre-timed versus actuated control for signals, free-flow speeds (measured versus estimated/assumed). Coding items, such as O-Ds, conditional turning movements, handling weave/merge/diverge, and node numbering convention are to conform to the NDOT Microsimulation Modeling Guidelines. HOV lanes, express lanes/managed lanes, and ramp meters are to be addressed. | $\checkmark$ |
| Calibration Approach | Calibration approach is to follow the methodologies described in the NDOT Microsimulation Modeling Guidelines. | N/A |
| Calibration MOEs, Locations, Targets | Calibration MOEs, locations to be calibrated and targets for acceptable match. | N/A |
| Selected MOEs for Evaluation | List of MOEs for evaluation and alternatives analysis along with the selected threshold for successful operations. Clearly state if intersection/arterial MOEs will be reported from Aimsun output or from the signal timing tool used. | $\checkmark$ |
| Additional item(s) | Any unique item(s) that is appropriate to be discussed/approved by NDOT. | $\checkmark$ |
| Comments: <br> The proposed methodology will not | port LOS corresponding to Aimsun outputs. |  |

## Attachment 2

Cursory Review of Year 2017 Existing Conditions Aimsun Next Scenarios in the l-515/l-215 FS Subarea

I-515/I-215 FS Subarea - Volume Comparison Results - Year 2017 AM Period

| Criteria | Acceptance Target | 7AM |  |  | 8AM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Points | Pass | Acceptance | Points | Pass | Acceptance |
| FLOW < 700, within 100 veh/h | > 85\% | 0 | 0 | \#N/A | 0 | 0 | \#N/A |
| 700 < FLOW < 2700, within 15\% | > 85\% | 5 | 5 | 100.0 | 5 | 5 | 100.0 |
| 2700 < FLOW < 5000, within 10\% | > 85\% | 3 | 3 | 100.0 | 4 | 4 | 100.0 |
| FLOW > 5000 within 250 veh/h | >85\% | 3 | 3 | 100.0 | 2 | 2 | 100.0 |
| GEH Statistic < 5 for individual link flows | > 85\% | 11 | 11 | 100.0 | 11 | 10 | 90.9 |
| GEH Statistic < 10 for individual link flows | 100\% | 11 | 11 | 100.0 | 11 | 11 | 100.0 |
| GEH Stastistic < 5 for all Turns | > 75\% | 62 | 42 | 67.7 | 62 | 45 | 72.6 |
| GEH Stastistic < 10 for all Turns | > 95\% | 62 | 51 | 82.3 | 62 | 53 | 85.5 |
| Percent GEH Passing | > 95\% | 73 | 62 | 84.9 | 73 | 64 | 87.7 |
| Sum of all link flows | > 95\% |  |  | 98.8 |  |  | 97.0 |




I-515/I-215 FS Subarea - Volume Comparison Results - Year 2017 PM Period

| Criteria | Acceptance Target | 4PM |  |  | 5PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Points | Pass | Acceptance | Points | Pass | Acceptance |
| FLOW < 700, within 100 veh/h | > 85\% | 0 | 0 | \#N/A | 1 | 1 | 100 |
| 700 < FLOW < 2700, within 15\% | > 85\% | 5 | 5 | 100.0 | 4 | 4 | 100.0 |
| 2700 < FLOW < 5000, within 10\% | > 85\% | 3 | 3 | 100.0 | 3 | 3 | 100.0 |
| FLOW > 5000 within 250 veh/h | >85\% | 2 | 2 | 100.0 | 2 | 2 | 100.0 |
| GEH Statistic < 5 for individual link flows | > 85\% | 10 | 7 | 70.0 | 10 | 7 | 70.0 |
| GEH Statistic < 10 for individual link flows | 100\% | 10 | 7 | 70.0 | 10 | 7 | 70.0 |
| GEH Stastistic < 5 for all Turns | > 75\% | 63 | 43 | 68.3 | 63 | 37 | 58.7 |
| GEH Stastistic < 10 for all Turns | > 95\% | 63 | 54 | 85.7 | 63 | 54 | 85.7 |
| Percent GEH Passing | > 95\% | 73 | 61 | 83.6 | 73 | 61 | 83.6 |
| Sum of all link flows | > 95\% |  |  | 85.1 |  |  | 78.8 |




I-515/l-215 FS Subarea - Speed Comparison Results - Year 2017 AM Period

| NRIX VS Aimsun Next |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | I215 EB E of Stephanie |  | 1215 WB W of Stephanie |  |
| $\begin{aligned} & \frac{x}{\alpha} \\ & \frac{z}{z} \end{aligned}$ | 7:00 AM | 65.4 | 53.7 | 60.6 | 65.8 |
|  | 7:15 AM | 65.1 | 51.2 | 50.9 | 64.8 |
|  | 7:30 AM | 64.6 | 49.0 | 34.7 | 64.7 |
|  | 7:45 AM | 64.6 | 45.9 | 29.5 | 66.6 |
|  | 8:00 AM | 64.6 | 47.3 | 44.9 | 65.1 |
|  | 8:15 AM | 64.5 | 45.6 | 54.0 | 65.7 |
|  | 8:30 AM | 65.1 | 49.5 | 52.9 | 66.2 |
|  | 8:45 AM | 64.0 | 49.1 | 51.7 | 65.4 |
|  | 7:00-9:00 | 64.7 | 48.9 | 47.4 | 65.5 |
|  | 7:00 AM | 64.6 | 46.4 | 61.6 | 63.3 |
|  | 7:15 AM | 64.6 | 46.5 | 61.7 | 62.9 |
|  | 7:30 AM | 63.6 | 46.1 | 59.7 | 62.2 |
|  | 7:45 AM | 63.6 | 46.3 | 60.4 | 62.7 |
|  | 8:00 AM | 64.2 | 46.6 | 60.8 | 63.3 |
|  | 8:15 AM | 64.5 | 46.4 | 62.1 | 63.2 |
|  | 8:30 AM | 64.6 | 46.8 | 62.6 | 63.2 |
|  | 8:45 AM | 64.6 | 46.6 | 62.1 | 63.0 |
|  | 7:00-9:00 | 64.3 | 46.4 | 61.3 | 63.0 |
|  | 7:00 AM | 0.8 | 7.3 | 1.0 | 2.5 |
|  | 7:15 AM | 0.5 | 4.7 | 10.8 | 1.9 |
|  | 7:30 AM | 1.0 | 2.9 | 25.0 | 2.5 |
|  | 7:45 AM | 1.0 | 0.3 | 30.9 | 3.9 |
|  | 8:00 AM | 0.3 | 0.7 | 15.9 | 1.8 |
|  | 8:15 AM | 0.0 | 0.8 | 8.0 | 2.5 |
|  | 8:30 AM | 0.5 | 2.7 | 9.7 | 3.0 |
|  | 8:45 AM | 0.5 | 2.5 | 10.4 | 2.4 |
|  | 7:00-9:00 | 0.5 | 2.5 | 13.9 | 2.6 |

I-515/l-215 FS Subarea - Speed Comparison Results - Year 2017 PM Period

| NRIX VSAME |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | I215 EB E of Stephanie |  | 1215 WB W of Stephanie |  |
| $\begin{aligned} & \frac{x}{o r} \\ & \underline{z} \end{aligned}$ | 4:00 PM | 48.7 | 47.2 | 56.9 | 63.9 |
|  | 4:15 PM | 53.0 | 48.8 | 52.5 | 63.4 |
|  | 4:30 PM | 58.7 | 52.3 | 54.6 | 64.5 |
|  | 4:45 PM | 58.9 | 49.4 | 57.5 | 63.7 |
|  | 5:00 PM | 54.7 | 48.1 | 60.7 | 64.9 |
|  | 5:15 PM | 51.1 | 47.0 | 58.0 | 64.2 |
|  | 5:30 PM | 52.3 | 47.3 | 56.2 | 63.3 |
|  | 5:45 PM | 51.8 | 49.9 | 59.5 | 63.8 |
|  | 4:00-6:00 | 53.6 | 48.7 | 57.0 | 64.0 |
|  | 4:00 PM | 49.6 | 45.1 | 61.2 | 61.5 |
|  | 4:15 PM | 13.1 | 45.6 | 62.1 | 61.9 |
|  | 4:30 PM | 9.0 | 44.4 | 60.9 | 61.5 |
|  | 4:45 PM | 9.5 | 44.7 | 61.6 | 61.4 |
|  | 5:00 PM | 8.2 | 43.4 | 61.2 | 61.6 |
|  | 5:15 PM | 7.9 | 44.0 | 61.9 | 61.4 |
|  | 5:30 PM | 8.2 | 43.8 | 60.7 | 61.4 |
|  | 5:45 PM | 7.9 | 44.6 | 58.6 | 61.8 |
|  | 4:00-6:00 | 17.8 | 44.4 | 61.0 | 61.6 |
|  | 4:00 PM | 0.9 | 2.1 | 4.3 | 2.3 |
|  | 4:15 PM | 39.8 | 3.2 | 9.6 | 1.5 |
|  | 4:30 PM | 49.7 | 7.9 | 6.3 | 3.0 |
|  | 4:45 PM | 49.4 | 4.7 | 4.2 | 2.3 |
|  | 5:00 PM | 46.5 | 4.7 | 0.5 | 3.3 |
|  | 5:15 PM | 43.2 | 3.0 | 3.9 | 2.8 |
|  | 5:30 PM | 44.1 | 3.4 | 4.5 | 1.9 |
|  | 5:45 PM | 43.9 | 5.3 | 1.0 | 2.0 |
|  | 4:00-6:00 | 35.9 | 4.3 | 4.0 | 2.4 |

## Attachment 3 <br> Year 2017 AM and PM Peak Hour Static Assignment Volumes

Appendix B

## Aimsun Next Model and other Associated Model Files (Provided Electronically)

 INTERCHANGEAppendix C Traffic Forecasting Guidelines Checklist

| No. | Item | Description | Check |
| :---: | :---: | :---: | :---: |
| 1 | Definitions | Terms used in your traffic forecast are in accordance with the definitions provided in the Traffic Forecasting Guidelines. | $\checkmark$ |
| 2 | Truth in Data Principle | The traffic forecast satisfies the requirements of the Truth in Data principle. | $\checkmark$ |
| 3 | Rounding Convention | The traffic forecast was developed adhering to the rounding convention. | $\checkmark$ |
| 4 | Methodology Memorandum | A methodology memorandum document was prepared and submitted to NDOT as per guidance offered in the Traffic Forecasting Guidelines. Any changes from the accepted methodology memorandum are documented clearly in the traffic forecasting report. | $\checkmark$ |
| 5 | Traffic Factors (Seasonal Factors, Axle Factors, AADT, $\mathrm{K}_{30}, \mathrm{D}_{30}, \mathrm{~T} \%$, etc.) | The traffic factors were obtained according to the guidance offered in the Traffic Forecasting Guidelines. | $\checkmark$ |
| 6 | Data Sources | The data sources were chosen according to the guidance offered in the Traffic Forecasting Guidelines. | $\checkmark$ |
| 7 | Adjusting $\mathrm{K}_{30}$ and $\mathrm{D}_{30}$ | $\mathrm{K}_{30}$ and $\mathrm{D}_{30}$ values were adjusted according to the guidance offered in the Traffic Forecasting Guidelines. | $\checkmark$ |
| Items 8 through 10 are relevant only if a travel demand model and the Traffic Forecasting Guidelines' Project Traffic Forecasting methodology was used for traffic forecasting. |  |  |  |
| 8 | Accuracy Levels | The accuracy levels listed in the Traffic Forecasting Guidelines were met or the necessary NCHRP Report 255 adjustments were performed. | N/A |
| 9 | Model Output Conversion Factor (MOCF) (if needed) | An MOCF was estimated to obtain AADT from model outputs. | N/A |
| 10 | Reasonableness Check with Historical Trend Projection | Historical trend projection was carried out to evaluate the reasonableness of the model projected volumes. | N/A |
| 11 | Historical Trend Projection | A historical trend projection analysis was carried out according to the guidance in the Traffic Forecasting Guidelines. | N/A |
| 12 | Constrained Facilities (if needed) | Guidance offered in the Traffic Forecasting Guidelines pertaining to constrained facilities was adopted. | $\checkmark$ |
| 13 | Peak Hour Volumes from DDHV | Peak hours of traffic were identified and the peak hour volumes were obtained from DDHV as per guidance offered in the Traffic Forecasting Guidelines. | N/A |
| 14 | Estimation of Intersection Turning Movements | Intersection turning movements were estimated following recommended methodologies. | N/A |
| 15 | Truck Traffic Forecasting | Truck traffic was forecast according to the guidance offered in the Traffic Forecasting Guidelines. | $\checkmark$ |
| Comments: |  |  |  | INTERCHANGE

Appendix D
Detailed Volume Calibration Results

| 7:00 to 8:00 AM |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Object | Count | Model | Absolute Difference | Relative Difference (\%) | GEH |
| 356272: RAMP US95 N AUTO SHO (24995) | 205 | 276.8 | 71.8 | 35.02439024 | 4.626004429 |
| 5982: 1215 (20221) | 6164 | 6475.1 | 311.1 | 5.047047372 | 3.913424269 |
| 13551: RAMP AUTO SHO US95 S (24996) | 177 | 227.8 | 50.8 | 28.70056497 | 3.570741888 |
| 6192: RAMP US95 N I215 W (24916) | 1057 | 1152.6 | 95.6 | 9.044465468 | 2.876179983 |
| 16078: RAMP I215E US95 (32349) | 1846 | 1959.5 | 113.5 | 6.148429036 | 2.601986244 |
| 17161: RAMP I215 E GIBSON (24911) | 719 | 789.6 | 70.6 | 9.819193324 | 2.570589014 |
| 13549: RAMP AUTO SHO US95 N (24994) | 387 | 341.7 | -45.3 | 11.70542636 | 2.373224456 |
| 13478: RAMP US95 S I215 W (24925) | 1764 | 1843.4 | 79.4 | 4.501133787 | 1.869555446 |
| 356271: RAMP S US95 AUTO SHO (21737) | 741 | 694.5 | -46.5 | 6.275303644 | 1.735666784 |
| 18244: RAMP US95S HORIZON (9771) | 788 | 836.9 | 48.9 | 6.205583756 | 1.715578274 |
| 13479: US 95 (24926) | 3317 | 3410.4 | 93.4 | 2.815797407 | 1.610416637 |
| 356194: RAMP I215 W VA VERDE (18802) | 408 | 439.3 | 31.3 | 7.671568627 | 1.520690148 |
| 356214: RAMP I125 W STEPHANI (20214) | 756 | 795.8 | 39.8 | 5.264550265 | 1.428828802 |
| 356240: RAMP US95 N E GALLER (24987) | 287 | 310.4 | 23.4 | 8.153310105 | 1.353936344 |
| 6164: RAMP US95N HORIZON (9842) | 203 | 187.6 | -15.4 | 7.586206897 | 1.101969563 |
| 6190: RAMP E I 215 US95 S (32347) | 3370 | 3429.2 | 59.2 | 1.756676558 | 1.015331351 |
| 5937: RAMP I215 W US95 S (24919) | 53 | 60.6 | 7.6 | 14.33962264 | 1.008415296 |
| 356267: RAMP US95 N SUNSET (8807) | 682 | 704.8 | 22.8 | 3.343108504 | 0.865850532 |
| 16985: US 95 (35378) | 2580 | 2537.9 | -42.1 | 1.631782946 | 0.832245002 |
| 5948: RAMP STEPHANI I215 W (20215) | 1330 | 1358.4 | 28.4 | 2.135338346 | 0.774615877 |
| 356263: RAMP US95 S SUNSET (8587) | 691 | 673.6 | -17.4 | 2.518089725 | 0.666133941 |
| 13472: RAMP I215 W GIBSON (24914) | 790 | 808.4 | 18.4 | 2.329113924 | 0.650863752 |
| 6727: RAMP SUNSET US95 N (8611) | 590 | 574.3 | -15.7 | 2.661016949 | 0.65070209 |
| 11194: I 215 (22244) | 5123 | 5166.8 | 43.8 | 0.854967792 | 0.610640551 |
| 6097: RAMP STEPHANI I215 E (20213) | 657 | 671.9 | 14.9 | 2.267884323 | 0.578036304 |
| 13477: RAMP US95S I215E (24924) | 664 | 678.4 | 14.4 | 2.168674699 | 0.555823005 |
| 5941: RAMP LK MEAD US95 N (15426) | 787 | 799.6 | 12.6 | 1.601016518 | 0.447354508 |
| 6016: RAMP VA VERDE I215 E (18806) | 446 | 438 | -8 | 1.793721973 | 0.380521195 |
| 6726: RAMP SUNSET US95 S (8740) | 375 | 380.2 | 5.2 | 1.386666667 | 0.267600765 |
| 17002: RAMP I215 W GIBSON (24913) | 553 | 547.7 | -5.3 | 0.95840868 | 0.225920887 |
| 13544: RAMP W GALLER US95 S (24991) | 364 | 368.1 | 4.1 | 1.126373626 | 0.214295796 |
| 6191: RAMP US95 E I 215 (12253) | 1451 | 1444.9 | -6.1 | 0.420399724 | 0.160307209 |
| 16075: RAMP GIBSON I215 E (32344) | 527 | 528 | 1 | 0.189753321 | 0.043540034 |
| 6206: RAMP HORIZON US95N (9774) | 1921 | 1922.9 | 1.9 | 0.098906819 | 0.043339366 |
| 5961: I 215 (20216) | 5474 | 5476.5 | 2.5 | 0.045670442 | 0.033786098 |
| Sum | 47247 | 48311.6 | -1064.6 | 97.75\% | 4.870421753 |


| 8:00 to 9:00 AM |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Object | Count | Model | Absolute Difference | Relative Difference (\%) | GEH |
| 13472: RAMP I215 W GIBSON (24914) | 677 | 751.2 | 74.2 | 10.96011817 | 2.776670772 |
| 13551: RAMP AUTO SHO US95 S (24996) | 224 | 267.4 | 43.4 | 19.375 | 2.768771725 |
| 6726: RAMP SUNSET US95 S (8740) | 436 | 383.9 | -52.1 | 11.94954128 | 2.573192506 |
| 6191: RAMP US95 E I 215 (12253) | 1068 | 1124.6 | 56.6 | 5.299625468 | 1.709431585 |
| 5937: RAMP I215 W US95 S (24919) | 73 | 60.9 | -12.1 | 16.57534247 | 1.478802172 |
| 6192: RAMP US95 N I215 W (24916) | 1063 | 1016.4 | -46.6 | 4.383819379 | 1.445213117 |
| 5948: RAMP STEPHANI I215 W (20215) | 1134 | 1167.7 | 33.7 | 2.971781305 | 0.993391729 |
| 16075: RAMP GIBSON I215 E (32344) | 408 | 428.3 | 20.3 | 4.975490196 | 0.992727351 |
| 13544: RAMP W GALLER US95 S (24991) | 272 | 287.5 | 15.5 | 5.698529412 | 0.926715977 |
| 6727: RAMP SUNSET US95 N (8611) | 563 | 541.7 | -21.3 | 3.78330373 | 0.906300927 |
| 356271: RAMP S US95 AUTO SHO (21737) | 516 | 497.7 | -18.3 | 3.546511628 | 0.812851786 |
| 16078: RAMP I215E US95 (32349) | 1758 | 1724.4 | -33.6 | 1.911262799 | 0.805220732 |
| 356267: RAMP US95 N SUNSET (8807) | 599 | 580.2 | -18.8 | 3.138564274 | 0.774246252 |
| 13549: RAMP AUTO SHO US95 N (24994) | 278 | 266 | -12 | 4.316546763 | 0.727606875 |
| 5982: 1215 (20221) | 5875 | 5826.9 | -48.1 | 0.818723404 | 0.628828017 |
| 356272: RAMP US95 N AUTO SHO (24995) | 263 | 272.2 | 9.2 | 3.498098859 | 0.562399302 |
| 5961: 1215 (20216) | 5237 | 5197.3 | -39.7 | 0.758067596 | 0.549634323 |
| 6190: RAMP E I 215 US95 S (32347) | 3204 | 3173.9 | -30.1 | 0.939450687 | 0.533018939 |
| 6164: RAMP US95N HORIZON (9842) | 193 | 186.6 | -6.4 | 3.316062176 | 0.464549364 |
| 18244: RAMP US95S HORIZON (9771) | 859 | 845.9 | -13.1 | 1.525029104 | 0.448680131 |
| 11194: I 215 (22244) | 4452 | 4481 | 29 | 0.651392633 | 0.433924657 |
| 17002: RAMP I215 W GIBSON (24913) | 397 | 388.7 | -8.3 | 2.090680101 | 0.41875954 |
| 13478: RAMP US95 S I215 W (24925) | 1659 | 1673 | 14 | 0.843881857 | 0.34299717 |
| 356194: RAMP I215 W VA VERDE (18802) | 407 | 413.2 | 6.2 | 1.523341523 | 0.306158841 |
| 16985: US 95 (35378) | 2143 | 2153 | 10 | 0.466635558 | 0.215765926 |
| 13477: RAMP US95S I215E (24924) | 593 | 588.1 | -4.9 | 0.826306914 | 0.201635847 |
| 356263: RAMP US95 S SUNSET (8587) | 609 | 604.3 | -4.7 | 0.771756979 | 0.190822138 |
| 356214: RAMP I125 W STEPHANI (20214) | 690 | 694.9 | 4.9 | 0.710144928 | 0.186209516 |
| 6097: RAMP STEPHANI I215 E (20213) | 630 | 634.6 | 4.6 | 0.73015873 | 0.182934762 |
| 356240: RAMP US95 N E GALLER (24987) | 253 | 250.4 | -2.6 | 1.027667984 | 0.163882183 |
| 6016: RAMP VA VERDE 1215 E (18806) | 421 | 424 | 3 | 0.712589074 | 0.145951277 |
| 6206: RAMP HORIZON US95N (9774) | 1552 | 1555.2 | 3.2 | 0.206185567 | 0.081185856 |
| 17161: RAMP I215 E GIBSON (24911) | 733 | 730.9 | -2.1 | 0.286493861 | 0.077620884 |
| 5941: RAMP LK MEAD US95 N (15426) | 639 | 637.2 | -1.8 | 0.281690141 | 0.071257098 |
| 13479: US 95 (24926) | 3348 | 3348.7 | 0.7 | 0.020908005 | 0.012097137 |
| Sum | 43226 | 43177.9 | 48.1 | 99.89\% | 0.23141601 |


| 4:00 to 5:00 PM |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Object | Count | Model | Absolute Difference | Relative Difference (\%) | GEH |
| 356272: RAMP US95 N AUTO SHO (24995) | 188 | 266.7 | 78.7 | 41.86170213 | 5.219480184 |
| 18244: RAMP US95S HORIZON (9771) | 1750 | 1969.6 | 219.6 | 12.54857143 | 5.092126853 |
| 13478: RAMP US95 S 1215 W (24925) | 2038 | 2194.9 | 156.9 | 7.698724239 | 3.410506936 |
| 5982: 1215 (20221) | 6428 | 6678.8 | 250.8 | 3.901680149 | 3.098091169 |
| 356240: RAMP US95 N E GALLER (24987) | 442 | 500 | 58 | 13.12217195 | 2.67249893 |
| 13479: US 95 (24926) | 4210 | 4379.4 | 169.4 | 4.023752969 | 2.584919304 |
| 6191: RAMP US95 E I 215 (12253) | 1208 | 1296.6 | 88.6 | 7.334437086 | 2.503684102 |
| 5961: 1215 (20216) | 6794 | 6598.5 | -195.5 | 2.877539005 | 2.389081317 |
| 356214: RAMP I125 W STEPHANI (20214) | 786 | 851.1 | 65.1 | 8.282442748 | 2.275403292 |
| 356194: RAMP 1215 W VA VERDE (18802) | 637 | 693.8 | 56.8 | 8.916797488 | 2.201947385 |
| 6190: RAMP E I 215 US95 S (32347) | 3971 | 3839.1 | -131.9 | 3.321581466 | 2.110724232 |
| 17002: RAMP I215 W GIBSON (24913) | 517 | 561.7 | 44.7 | 8.646034816 | 1.924740486 |
| 6192: RAMP US95 N I215 W (24916) | 1069 | 1122.4 | 53.4 | 4.995322732 | 1.613226793 |
| 13472: RAMP I215 W GIBSON (24914) | 862 | 903.1 | 41.1 | 4.767981439 | 1.383477697 |
| 6726: RAMP SUNSET US95 S (8740) | 884 | 846.1 | -37.9 | 4.287330317 | 1.288601417 |
| 16985: US 95 (35378) | 2392 | 2453.3 | 61.3 | 2.56270903 | 1.245417995 |
| 16078: RAMP I215E US95 (32349) | 1942 | 1894.4 | -47.6 | 2.451081359 | 1.086825975 |
| 13551: RAMP AUTO SHO US95 S (24996) | 364 | 381.8 | 17.8 | 4.89010989 | 0.921772634 |
| 5941: RAMP LK MEAD US95 N (15426) | 668 | 690.9 | 22.9 | 3.428143713 | 0.878530272 |
| 356263: RAMP US95 S SUNSET (8587) | 820 | 796.8 | -23.2 | 2.829268293 | 0.815971204 |
| 13549: RAMP AUTO SHO US95 N (24994) | 586 | 567.7 | -18.3 | 3.122866894 | 0.761938013 |
| 356267: RAMP US95 N SUNSET (8807) | 770 | 790.8 | 20.8 | 2.701298701 | 0.744568578 |
| 13477: RAMP US95S I215E (24924) | 906 | 928.5 | 22.5 | 2.483443709 | 0.742914197 |
| 6165: RAMP HORZON US95 S (9844) | 234 | 227 | -7 | 2.991452991 | 0.461065445 |
| 13544: RAMP W GALLER US95 S (24991) | 480 | 488.7 | 8.7 | 1.8125 | 0.395311638 |
| 5948: RAMP STEPHANI I215 W (20215) | 1277 | 1290.3 | 13.3 | 1.041503524 | 0.371217403 |
| 5937: RAMP I215 W US95 S (24919) | 137 | 140.9 | 3.9 | 2.846715328 | 0.330853194 |
| 6097: RAMP STEPHANI I215 E (20213) | 733 | 741.7 | 8.7 | 1.186903138 | 0.320392551 |
| 356271: RAMP S US95 AUTO SHO (21737) | 547 | 553.5 | 6.5 | 1.188299817 | 0.277097962 |
| 17161: RAMP I215 E GIBSON (24911) | 827 | 820.4 | -6.6 | 0.798065296 | 0.229963761 |
| 6164: RAMP US95N HORIZON (9842) | 187 | 184 | -3 | 1.604278075 | 0.220266929 |
| 6016: RAMP VA VERDE I215 E (18806) | 395 | 398.6 | 3.6 | 0.911392405 | 0.180724349 |
| 16075: RAMP GIBSON I215 E (32344) | 416 | 418.9 | 2.9 | 0.697115385 | 0.141937047 |
| 6727: RAMP SUNSET US95 N (8611) | 918 | 921.3 | 3.3 | 0.359477124 | 0.108818479 |
| 6206: RAMP HORIZON US95N (9774) | 1097 | 1098.4 | 1.4 | 0.127620784 | 0.042255788 |
| 356207: RAMP I215 E STEPHANI (20212) | 1246 | 1244.9 | -1.1 | 0.088282504 | 0.031169479 |
| Sum | 48726 | 49734.6 | -1008.6 | 97.93\% | 4.545720434 |


| 5:00 to 6:00 PM |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Object | Count | Model | Absolute Difference | Relative Difference (\%) | GEH |
| 356272: RAMP US95 N AUTO SHO (24995) | 240 | 276.6 | 36.6 | 15.25 | 2.277292848 |
| 356271: RAMP S US95 AUTO SHO (21737) | 514 | 482.7 | -31.3 | 6.089494163 | 1.402093921 |
| 16078: RAMP I215E US95 (32349) | 1942 | 1882 | -60 | 3.089598352 | 1.372168061 |
| 13549: RAMP AUTO SHO US95 N (24994) | 546 | 518.6 | -27.4 | 5.018315018 | 1.187605854 |
| 16075: RAMP GIBSON I215 E (32344) | 367 | 387.4 | 20.4 | 5.558583106 | 1.050374876 |
| 16985: US 95 (35378) | 2410 | 2453.4 | 43.4 | 1.800829876 | 0.880105494 |
| 356263: RAMP US95 S SUNSET (8587) | 745 | 726.5 | -18.5 | 2.483221477 | 0.682034892 |
| 356214: RAMP I125 W STEPHANI (20214) | 737 | 719.7 | -17.3 | 2.347354138 | 0.641026584 |
| 6097: RAMP STEPHANI I215 E (20213) | 727 | 744 | 17 | 2.338376891 | 0.626841271 |
| 5961: 1215 (20216) | 6648 | 6697.1 | 49.1 | 0.73856799 | 0.601084562 |
| 5982: 1215 (20221) | 6178 | 6131.6 | -46.4 | 0.75105212 | 0.591440429 |
| 6192: RAMP US95 N I215 W (24916) | 1030 | 1012.1 | -17.9 | 1.737864078 | 0.560182485 |
| 6016: RAMP VA VERDE 1215 E (18806) | 400 | 410.3 | 10.3 | 2.575 | 0.511716361 |
| 356267: RAMP US95 N SUNSET (8807) | 750 | 763.2 | 13.2 | 1.76 | 0.479888964 |
| 13551: RAMP AUTO SHO US95 S (24996) | 448 | 458.2 | 10.2 | 2.276785714 | 0.479184918 |
| 5948: RAMP STEPHANI I215 W (20215) | 1288 | 1304.7 | 16.7 | 1.296583851 | 0.463826262 |
| 17161: RAMP I215 E GIBSON (24911) | 858 | 871.5 | 13.5 | 1.573426573 | 0.459080116 |
| 6164: RAMP US95N HORIZON (9842) | 187 | 193.1 | 6.1 | 3.262032086 | 0.442482295 |
| 13478: RAMP US95 S I215 W (24925) | 2005 | 2021.8 | 16.8 | 0.837905237 | 0.37440725 |
| 6726: RAMP SUNSET US95 S (8740) | 835 | 824.3 | -10.7 | 1.281437126 | 0.371480754 |
| 356207: RAMP I215 E STEPHANI (20212) | 1304 | 1315.3 | 11.3 | 0.866564417 | 0.31224883 |
| 5937: RAMP I215 W US95 S (24919) | 120 | 123.4 | 3.4 | 2.833333333 | 0.308200705 |
| 6191: RAMP US95 E 215 (12253) | 1155 | 1145 | -10 | 0.865800866 | 0.294883912 |
| 13479: US 95 (24926) | 4496 | 4513.4 | 17.4 | 0.387010676 | 0.259248535 |
| 13477: RAMP US95S I215E (24924) | 1096 | 1087.8 | -8.2 | 0.748175182 | 0.248154651 |
| 6165: RAMP HORZON US95 S (9844) | 306 | 310 | 4 | 1.307189542 | 0.227921153 |
| 6206: RAMP HORIZON US95N (9774) | 1126 | 1118.6 | -7.4 | 0.657193606 | 0.220890602 |
| 356194: RAMP I215 W VA VERDE (18802) | 628 | 633 | 5 | 0.796178344 | 0.199125766 |
| 356240: RAMP US95 N E GALLER (24987) | 454 | 451.1 | -2.9 | 0.63876652 | 0.136321612 |
| 6727: RAMP SUNSET US95 N (8611) | 771 | 774.6 | 3.6 | 0.46692607 | 0.129499754 |
| 17002: RAMP I215 W GIBSON (24913) | 555 | 557.6 | 2.6 | 0.468468468 | 0.110234825 |
| 13544: RAMP W GALLER US95 S (24991) | 436 | 438.2 | 2.2 | 0.504587156 | 0.105228233 |
| 6190: RAMP E I 215 US95 S (32347) | 4074 | 4078.8 | 4.8 | 0.117820324 | 0.07518009 |
| 18244: RAMP US95S HORIZON (9771) | 1845 | 1847.7 | 2.7 | 0.146341463 | 0.062835742 |
| 5941: RAMP LK MEAD US95 N (15426) | 679 | 679.9 | 0.9 | 0.132547865 | 0.034527391 |
| 13472: RAMP I215 W GIBSON (24914) | 859 | 858.8 | -0.2 | 0.023282887 | 0.006824309 |
| Sum | 48759 | 48812 | -53 | 99.89\% | 0.239955379 |

Appendix E


Appendix F Memorandum


## 2040 Micro/Meso Future Volume Development Technical Memorandum

September 2018

# 2040 Micro/Meso Future Volume Development Technical Memorandum <br> for Southern Nevada Traffic Study 

Prepared for:
TEEVADA

Prepared by:
$1-32$

September 2018
SOUTHERN NEVADA TRAFFIC STUDY
2040 Micro/Meso Future Volume Development Technical Memorandum
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## INTRODUCTION

This document outlines the approach used to develop 2040 future traffic volumes for the Southern Nevada Traffic Study (SNTS), using standard methodologies to adjust the demand matrices outside of the Aimsun and TransCAD software packages. Input demand data sets were based on the Regional Transportation Commission of Southern Nevada's (RTCSNV) TransCAD travel demand model. Traffic counts collected in the field were used to create calibrated base year 2017 ("adjusted") traffic volumes for the study. This document describes the methodology used to apply the growth patterns forecasted by the RTCSNV TransCAD model to the calibrated 2017 adjusted matrix to develop a refined or "adjusted" 2040 set of traffic forecast volumes.

This document also provides an overview of why these methodologies were necessary and the benefits of the methodology selected.

## 2040 MICRO/MESO FUTURE VOLUME DEVELOPMENT

2040 "No-Build" macro-level future volume matrices were created using TransCAD and imported into Aimsun Next in the same manner as the 2017 matrices (as described in section 4.3 of the 2017 Aimsun Next Model Development and Calibration Report). The macro-level TransCAD assignment volumes provided an initial demand set. However, it is standard industry practice to post-process travel demand model demand matrices by referencing observed field traffic counts in the base year. These postprocessing adjustments are applied in the future year to produce refined traffic forecasts that are suitable for micro/meso analysis. The Aimsun software was not capable of providing these refined/post-processed demand sets. Thus, a methodology was developed that utilized the calibrated/adjusted 2017 traffic flows and the unique forecasted traffic patterns from the TransCAD model for the SNTS study area to establish refined/adjusted 2040 traffic volume forecasts.

The process of creating individual calibrated 2017 subnetwork matrices (as outlined in section 4.3 of the 2017 Aimsun Next Model Development and Calibration Report) required a combination of creating subnetwork traversals and origin-destination (O-D) matrix adjustments. However, a new process was required to develop refined forecasts of 2040 future volume matrices.

Two methods were tested for development of the refined 2040 future volume matrices. The terms defined below are used in the discussion of the two methods.

- 2017 Unadjusted-A matrix that represents the subnetwork 2-hour O-D traversals that were created based on the full network 2017 TransCAD assignment using Aimsun Next static assignment process. These reflect "unadjusted" matrices as the full network matrices were taken directly from TransCAD output.
- 2017 Adjusted-A matrix that represents the product of O-D adjustments at the subnetwork level. The matrices were "adjusted" through an O-D matrix estimation (ODME) approach that refines individual O-D volume pairs to better fit observed traffic counts on subnetwork turns and sections.
- 2040 Unadjusted—A matrix that represents the subnetwork 2-hour O-D traversals (similar to the 2017 Unadjusted), that were generated based on the full network 2040 TransCAD assignment volumes. The


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development of these matrices was created by running traversals of specific subnetworks based on the 2040 TransCAD full network matrices. No O-D adjustments were ran on "Unadjusted" matrices.

- 2040 Adjusted—A matrix that represents the refined "finished product" that was the result of applying the preferred matrix growth methodology detailed below.


## Iterative Proportional Fitting Method

Sometimes referred to as the 'Raking' method, the Iterative Proportional Fitting (IPF) Method is an iterative procedure for adjusting a table of data cells such that they add up to the selected totals for both the columns and rows of the table. The unadjusted values in each data cell are referred to as the 'seeds' and the selected totals are referred to as the 'marginal' totals. Figure 1 shows an example of what the IPF Method looks like before and after application to a matrix.

Figure 1. Example of IPF Application


As illustrated in Figure 1, the row and column totals of the seeds from the "Before" matrix seed cells do not match the desired "selected" column and row marginal totals. The IPF Method adjusts the individual cell values, using the seeds as the starting point, until all row and column sums are equal to, or are as close as possible to, the desired marginal totals.

In the case of the SNTS study, the "Before" matrix was the 2017 unadjusted matrix and the "After" matrix was the 2017 adjusted matrix. A flow chart of how the IPF Method was applied to the SNTS study is presented in Figure 2.

Figure 2. Illustration of Potential IPF Approach Framework for the SNTS Study


The IPF is a methodology that has been used in travel modeling for many years, and the results of the IPF Method are acceptable and reasonable at the macro level. The IPF methodology focuses on the "margin" for its growth-factoring approach, meaning that, it applies a growth factor according to the growth of all origins or destinations for that zone. It does not focus on the individual zone-to-zone growth patterns reflected between the 2017 and 2040 Unadjusted matrices. When applied for the SNTS study area, the IPF Method application provided a set of matrices that were passable. However, this method did not result in an optimal match when comparing the total growth rates of the 2040 Adjusted to 2017 Adjusted matrices. Because of the methodological issue identified above, and the imprecision of the IPF application results, a zone-to-zone growth percentage, or "Pivot-Point" Method, was tested and applied.

## Pivot-Point Method

The modified Pivot-Point Method established an enhanced base-year matrix and then "pivots" off that enhanced base-year matrix based on unique zone-to-zone growth characteristics. The zone-to-zone change in tripmaking came from the RTCSNV regional model's base year model and future year model unadjusted matrices. The technique takes advantage of the adjusted base year matrix, which was refined with available traffic counts, while maintaining the regional model's zone-to-zone future tripmaking patterns and changes. In this case, the purpose is to "pivot" from a fixed base year matrix (the 2017 Adjusted matrix) by adjusting individual cells of the matrix according to unique levels of growth identified by the TransCAD unadjusted matrices for 2017 and 2040. A flow chart of the modified Pivot-Point Method is presented in Figure 3.

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Figure 3. Potential Pivot-Point Approach Framework for the SNTS Study

*15\% threshold for deviation between base year unadjusted and adjusted
**Matrix Adjustment applied to each individual OD pair
All calculations are performed for each OD pair (individual cell)

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The modified Pivot-Point Method combines elements of absolute (or additive) matrix adjustments and relative (or multiplicative) matrix adjustments. In instances where there were large matrix corrections between the 2017 Unadjusted and Adjusted matrices, there can be a tendency for a purely relative/multiplicative factor to skew growth unreasonably high. The following is a hypothetical situation for a single matrix cell between two zones $i$ and $j$ (also called an " $i-j$ pair"):

- The TransCAD model estimates only 1 trip between zones i and j for 2017 (this is the 2017 Unadjusted matrix value).
- Based on observed data, the adjusted matrix indicates 100 trips between zones $i$ and $j$ for 2017 (this is the 2017 Adjusted matrix value).
- The TransCAD model estimates 2 trips between zones i and j for 2040 (this is the 2040 Unadjusted matrix value).

In this case, because of high levels of base year deviation between unadjusted and adjusted, using a relative/multiplicative factor would indicate 200 trips between zones i and j for 2040 (because of the growth factor of 2.0—1 trip in 2017 doubled to 2 trips in 2040).

For this reason, a 15 percent threshold was applied for use of a relative/multiplicative factor for creating the 2040 Adjusted matrix. Thus, in developing the unique 2040 Adjusted matrix cell values:

- For all i-j pairs where the 2017 Unadjusted and Adjusted values deviated by more than 15 percent, only an absolute trip adjustment was applied to the 2040 Unadjusted matrix. This means, in the example above, instead of doubling the number of 2017 Adjusted trips (100 trips in $2017 \times 2.0=200$ trips in 2040), the Pivot-Point Method would add 1 trip (100 trips in $2017+1$ new trip $=101$ trips in 2040).
- For all i-j pairs where the 2017 Unadjusted and Adjusted values deviate by 15 percent or less, the average of the absolute (using addition) and relative (using multiplication) trip corrections was applied to the 2040 Unadjusted matrix.

This is similar to a link-based forecasting methodology applied in NCHRP 255 (now updated as NCHRP 765).

The calculations described in Figure 3 are performed for each i-j pair of the matrix. An example of the modified Pivot-Point Method is presented in Figure 4.

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Figure 4. Example of Pivot-Point Approach Methodology
Unadjusted TransCAD Volumes


Change to 2017 Adjusted


## 2040 Adjusted Methods



## Initial 2040 Adjusted



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Figure 4. Example of Pivot-Point Approach Methodology
Final 2040 Adjusted


All Steps

|  | Original TCAD Model (Unadjusted) |  |  |  | 2017 Adjusted(Based on Traffic Counts) |  |  | 2040 Adjusted Trips (via Different Methods) |  | Initial 2040 Adjusted |  | Final 2040 Adjusted |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2017 ij Trips | 2040 ij Trips | \% Growth | Absolute Growth | $\begin{gathered} \hline \text { Final } 2017 \text { ij } \\ \text { Trips } \\ \hline \end{gathered}$ | \% Deviation | Absolute Deviation | \%Growth Method | Abs Growth Method | Method Description | $\begin{array}{\|c\|} \hline \begin{array}{c} \text { Initial } 2040 \mathrm{ij} \\ \text { Trips } \end{array} \\ \hline \end{array}$ | Target Adjustment | $\begin{array}{\|c\|} \hline \text { Final } 2040 \mathrm{ij} \\ \text { Trips } \\ \hline \end{array}$ |
| Example 1 | 25 | 75 | 200\% | 50 | 50 | 100\% | 25 | 150 | 100 | \% Deviation > 15\%, so ABSOLUTE GROWTH | 100 | -5\% | 95 |
| Example 2 | 100 | 200 | 100\% | 100 | 110 | 10\% | 10 | 220 | 210 | $\begin{gathered} 15 \%>\% \text { Deviation }>-15 \%, \\ \text { so } \\ \text { AVERAGE } \end{gathered}$ | 215 | -5\% | 204 |

## CONCLUSION

Although both methods provide acceptable results, the Pivot-Point Method provided the best representation for 2040 No-Build volume matrices compared to the IPF Method.

The main benefit of the Pivot-Point Method is its ability to maintain the unique zone-to-zone growth patterns identified by the TransCAD model. In this respect, a negative aspect of the IPF Method is that, it implements a "margin-based" approach, where a single origin or destination factor is applied to all origins or destinations for each zone.

A second benefit of the Pivot-Point Method is its ability to employ a 15 percent deviation factor, which limits any multiplicative growth factors only to those matrix cells that have a good base year fit between the TransCAD model and observed counts. This eliminates the issue of a traffic movement having an unreasonably high multiplicative factor applied to it in situations where the model is under-estimating or over-estimating demand.

## Appendix G

## Future Year 2040 AADTs









| AADT (ypd) | 56,500 | 18,000 | 38,500 | 25,500 | 51,000 | 23,500 | 35,000 | 5,100 | 40,000 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NB $1-515$ <br>  <br> SB $1-515$ |  |  |  |  |  |  |  |  |  |  |
| AADT (vpd) | 27,000 | 3,200 | 28,000 | 36,500 | 72,000 | 32,500 | 39,000 | 5,200 | 44,000 |  |







[^0]:    ${ }^{1}$ The I-515/I-215 Interchange Feasibility Study: Traffic Operations Methodology Memorandum was submitted to NDOT on January 28, 2019 and was approved by NDOT on February 4, 2019.

[^1]:    ${ }^{2}$ The year 2040 OD matrices for the I-515/I-215 FS subarea were obtained as explained in Section 4.2.

[^2]:    ${ }^{1}$ The current Southern Nevada Aimsun Next model does not have any dynamic scenarios for the SNTS' I-215/l-515 subarea.

